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5 BACKGROUND OF THE INVENTION

The present Invention relates to a dry etching method used for fine manufacturing of semiconductor devices, particularly, to a dry etching method for realizing high-precision dry etching manufacturing of
10 silicon oxide film.

In order to connect electrically transistor structures formed on a wafer with metallic circuits to be connected, and to connect electrically the metallic circuits each other, contact holes are formed in an
15 insulating film (it means a thin film containing SiO_2 as a main component, or a material having a low dielectric constant (Low-K film) such as an organic film, and it is called as an oxide film, hereinafter), and the contact holes are filled with an electric
20 conductor. In accordance with the dry etching process, the contact holes are formed by the steps of introducing an etching gas into a vacuum chamber, generating a plasma by applying high frequency waves, or microwaves to the etching gas, and etching the oxide
25 film selectively with active species and ions generated in the plasma. During the etching process, a resist thin film being reprinted with a hole pattern is formed

on the oxide film. In accordance with the contact holes manufacturing, the oxide film must be etched selectively to the resist film, a circuit layer under the contact holes, and silicon forming the transistors. Moreover, in accordance with a dry etching method; wherein gate electrodes of field-effect transistor formed on a wafer are covered with a second insulating film made of a material different from the insulating film between the circuit layers, and a source region and a drain region are connected to the circuit layer; a selectivity of the second insulating film is required, because the second insulating film is appeared in the contact holes during the etching process. The contact manufacturing is called as a self-aligning contact (SAC), and a silicon nitride film is used as the second insulating film.

The contact holes manufacturing is performed by the steps of introducing fluorocarbon gases such as CF_4 , CHF_3 , C_4F_8 , C_4F_6 , C_5F_8 , and Ar gas into an etching apparatus, and etching the wafer under a condition, wherein a bias voltage (V_{pp} voltage) of 1.5-2.0 kV is applied to the wafer, by high frequency plasma discharging in a gas pressure condition of 4 Pa-10 Pa. When the thickness of the oxide film between the circuit layers is thick, and an aspect ratio (a ratio of depth/diameter) of the contact hole is high, oxygen

gas has been added in order to increase an aperture of the hole, and CO gas has been added in order to increase selectivity of the resist and the silicon nitride film.

- 5 In examples other than the oxide film etching, for example in manufacturing of the gate electrode, a mixed gas of chlorine gas, hydrogen bromide gas, and oxygen gas has been used. Anisotropic manufacturing has been controlled by adding oxygen. However, when
- 10 polycrystalline Si of p-type and n-type are contained in a material for the gate electrode, side planes of n-type polycrystalline Si are etched by Cl radicals and Br radicals, and it is difficult to obtain the same manufactured shape as the p-type polycrystalline Si.
- 15 In manufacturing wiring materials such as TiN and Al-Cu alloys, a mixed gas of chlorine gas and boron chloride gas is used as the etching gas, and hydrocarbon gas and a hydrocarbon gas, of which hydrogen is partly substituted with fluorine, or nitrogen gas are added,
- 20 in order to control its anisotropic manufacturing. Although these additive gases form a protective film against highly reactive Cl radicals, these additive gases cause a problem to grow shapes of isolated patterns. In the process of oxide film etching, the
- 25 etching characteristics are determined by CF_2 , F, and ions in the plasma. (In plasma of CF group gas, CF, CF_3 , C_2 , and the like are existing in addition to CF_2 .)

However, in the present specification, C, CF, CF₃, and the like are represented by CF radicals, and CF₂ radical is expressed as CF₂, and F radical is expressed as F.) More exactly, the etching characteristics
5 depend on a generating amount of F and ions to CF₂ in the plasma. The reason is as follows:

Fluorocarbon gas introduced into an etching treatment chamber is dissociated to CF₂ radical, F radical, and ions in plasma, and injected into the
10 wafer. Etching of the oxide film is proceeded by injecting ions onto planes whereon CF₂ and F are adhered. On the contrary, etching of resist or silicon nitride film is proceeded by F and ions, and CF₂ operates as an anti-etching film on the resist or the
15 silicon nitride film by forming a polymer on their surface. Therefore, if the etching operation is performed under a condition wherein the injecting amounts of ions and F are smaller than that of CF₂, a high selection ratio to the resist or the silicon
20 nitride film can be obtained. However, if the injecting amount of the ions is decreased, a problem that the etching velocity of the oxide film is decreased is generated. If the injecting amount of F is decreased, a problem that the etching process is terminated at holes
25 having a high aspect ratio is generated. As explained above, the etching process is determined by the injection of CF₂, F, and ions, and, in particular, the

etching process depends on the Injecting amounts of ions and F to the injecting amount of CF_2 . Accordingly if the generating amount of F and ions to CF_2 in the plasma can be controlled independently, the process condition is extended, and as the result, finer and deeper manufacturing of the oxide film than ever becomes possible. Precisely, the etching velocity and selection ratio are influenced by the kind of the ions, but fundamentally, the etching process is determined by the amount of the F and the ions to the CF_2 . When Ar diluting gas is used, almost of the partial pressure is based on the Ar gas, and almost of the ions are Ar ions. When the Ar diluting gas is not used, CF ions and C ions are injected. However, the amounts of the ions are 1/100-1/10 in comparison with the total amount of the radicals. The selectivity and the etching velocity are influenced by the kind of the ions, and an optimum generating amount of F to CF_2 is shifted sometimes approximately 10 per cent. Because the etching process is controlled by the mechanism explained above, a polymer is formed at the bottom of the contact hole with the CF radicals, and the etching process is terminated at a middle point, when the contact holes having a high aspect ratio are manufactured under an etching condition that F is less so as to obtain a high aspect ratio, because F becomes less at the bottom portion of the contact holes. On

the contrary, in a case under a condition wherein a plenty of F and oxygen are supplied and the etching is not terminated, F and oxygen are supplied sufficiently to the bottom portion of the contact holes, and the etching process is proceeded. However, because the resist mask is etched with an excess of F and oxygen, the selection ratio to the resist can not be obtained sufficiently. Therefore, in accordance with the etching process to the contact holes explained above, an optimization of the injecting amount of ions and the injecting amount of F to the injecting amount of CF_2 is necessary. However, in accordance with conventional etching apparatus, the yielding amounts of F, CF_2 , and ions by dissociation of CF group etching gas are fixed, because a plasma density and an electronic temperature are fixed by determining an etching condition such as gas pressure, a high frequency power necessary for generating the plasma, and so on. Therefore, it has been difficult to change the generating amount of the ions with maintaining the generating amounts of F and CF_2 are constant, or to change the injecting amount of the F and CF_2 under a condition that the generating amounts of the ions is constant. For instance, in a case of a parallel plates type etching apparatus, the generating amount of the ions is increased by increasing a high frequency bias power for generating plasma, because the plasma density is increased.

Simultaneously, the generating amount of F to CF₂ is also changed, because the dissociation by the plasma is proceeded.

Therefore, in accordance with the conventional art, the problem could not be solved, because the gas dissociation in the plasma was fixed, and the kinds, ratio, and generating amount of the radicals could not be controlled freely.

Additionally, when the contact holes having a high aspect ratio are etched under a condition wherein the gas pressure is as high as the prior art, the ions which should be injected perpendicularly into the wafer are collided with gas molecules, because the gas pressure is high, and a plenty of the ions are injected into the wafer in a slant direction. Therefore, the perpendicular manufacturing becomes difficult, because a part of the oxide film is manufactured in a lateral direction. The collision of the ions with the gas molecules can be prevented by decreasing the gas pressure, but in accordance with the conventional apparatus, if the gas pressure is decreased, the plasma density and the electronic temperature are changed. Accordingly, the decreasing the gas pressure has caused a problem that the ratio of F is increased, and a sufficient selection ratio to the resist and the nitride film can not be obtained. In accordance with miniaturizing semiconductor devices, the etching

process of the oxide film is required to be improved in preciseness of the manufacturing, and in the selection ratio to the nitride film (a nitride film selection ratio) and the selection ratio to the resist. In accordance with flattening the semiconductor device and increasing the multi-layered circuits, manufacturing the contact holes having a high depth/hole diameter ratio (aspect ratio) has been required.

The problem to be solved by the present invention is to realize manufacturing the oxide film, wherein a high selection ratio is required to the contact holes having a high aspect ratio and silicon nitride film, by controlling the generating amount of F and ions to CF_2 in plasma.

Furthermore, in manufacturing the gate electrode and the metallic circuit, the side etching by injecting Cl radicals and Br radicals into side planes of the pattern becomes a problem. The problem to be solved by the present invention includes an improvement in anisotropic manufacturing the gate electrode and the metallic circuit.

Furthermore, not restricted to the semiconductor wafer used for manufacturing the oxide film, the gate electrode and the metallic circuit, the present invention is aimed at realizing the anisotropic manufacturing by readily setting, or controlling etching active species, the amount of the ions, and

ratio, which are optimum for the manufacturing, to various substrates (members to be manufactured) including liquid crystal substrates, DVD substrates, glass substrates, and so on.

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SUMMARY OF THE INVENTION

In order to solve the above problems of the present invention, controlling and adjusting
10 independently the generating amount of the radicals and the amount of the ions in the plasma are necessary. As a means therefor, the present invention sets an optimum electronic temperature region in the plasma. Or the present invention controls the electronic temperature
15 region. The generating amounts of F and ions to CF_2 in plasma can be controlled independently by forming at least two plasma regions having different electronic temperature each other. In accordance with oxide film etching process using fluorocarbon gas, the generating
20 amount of F to CF_2 is determined depending on the plasma temperature, and the generating amount of the ions are determined in proportional to the power introduced into the plasma generation. In a case of C_4F_8 , the threshold energy for generating F from C_4F_8 is
25 approximately 6 eV, but generation of CF_2 requires approximately 12 ev. Therefore, in a case when the electronic temperature is low (1-4eV), F is readily

formed, and a CF_2/F generating ratio becomes small.

When the electronic temperature is in the range of 5-20 eV, generation of CF_2 is enhanced, and the CF_2/F generating ratio becomes larger in comparison with the case of the low electronic temperature. Then, if two kinds of electronic temperature are used, it becomes possible to generate F and CF_2 at the high electronic temperature region, and to generate mainly F at the low temperature region. Accordingly, the generating amounts of F and CF_2 can be controlled or adjusted by setting appropriate values of the electronic temperature. In a condition wherein the values of the high and low electronic temperature are set, a CF_2/F ratio can be controlled by changing the areas of the two electronic temperature regions. The difference of these electronic temperature is at least 1 eV, preferably at least 5 eV. The two electronic temperature regions are spatially continued. The high electronic temperature region described hereinafter means a peak at the maximum value of the electronic temperature and its peripheral region, and a peripheral portion of a portion, wherein the electronic temperature becomes maximum, on a member to be treated or between the center in the member to be treated and a facing plane to the member to be treated. A position whereat the electronic temperature becomes an average value of the high electronic temperature and the low

electronic temperature between the member to be treated and the facing plane to the member to be treated is defined as a boundary between the high electronic temperature region and the low electronic temperature region. If each of the low electronic temperature regions exists at both sides of the high electronic temperature region, a second boundary between the high electronic temperature region and the low electronic temperature region is defined additionally as same as the previous boundary. Here, the lowest electronic temperature in the second low electronic temperature region is equal to or somewhat higher than the lowest electronic temperature in the first low electronic temperature region. In a case when two electronic temperature regions are formed such as the present invention, F is generated in both the two electronic temperature regions, and the ratio of CF_2/F is controlled in a condition where the total F exists excessively. The F can be eliminated selectively by adding a gas including hydrogen atom (such as H_2 , CF_2F_2 , CH_4 and so on) so as to react the F with H radicals. Furthermore, the F can be consumed by a reaction with inner wall materials. Practically, the inner wall of the etching apparatus is composed of the materials, which reacts with F, such as Si plate, SiC plate and the like, and F is eliminated by applying high frequency bias to the plates in order to enhance the

consumption of F. Furthermore, the F can be eliminated by reacting with a polymer formed by adhering CF_2 onto the inner wall. If the wafer is placed closer to the inner wall portion, an injection fraction of F, which
5 is generated by the plasma in the etching apparatus, into the inner wall is increased, because the area of the inner wall to the volume of the plasma is increased. That is, F can be eliminated effectively with reactions with the polymer by placing the wafer
10 closer to the inner wall portion. Practically, a distance between the wafer and a plane facing to the wafer of the etching apparatus is shortened. In accordance with using the above means with the plasma having two kinds of electronic temperature, the ratio
15 of CF_2/F becomes possible to be controlled in a wide range.

On the contrary, the generating amount of the ions is determined by the electronic density in the plasma, and the electronic density is approximately
20 proportional to the high frequency input power. Individual radical (CF_2 , F) is increased with increase of the high frequency power, but the generation ratio of CF_2/F scarcely depend on the high frequency power. Accordingly, making the two electronic temperature
25 regions variable, the generating amount of the ions is maintained constant and the generation ratio of CF_2/F can be controlled independently. Furthermore the

generating amount of CF_2 depends on the gas flow rate or partial pressure of fluorocarbon gas, and an injection ratio of CF_2 /ions into the member to be treated can be controlled by the high frequency power
5 in a condition wherein the dissociation of fluorocarbon to CF_2 is saturated.

BRIEF DESCRIPTION OF THE DRAWINGS

- 10 FIG. 1 is a cross section of the dry etching apparatus using in the present invention, and a conceptual illustration indicating a formation of two kinds of electronic temperature regions of the present invention,
- 15 FIG. 2 is an illustration indicating a relationship between magnetic field intensity of ECR used in the present invention versus magnetic gradient and a thickness of the high electronic temperature region,
- 20 FIG. 3 is an illustration indicating a relationship between formation of two kinds of electronic temperature regions by controlling the magnetic gradient of the present invention versus the generation ratio of CF_2/F ,
- 25 FIG. 4 is an illustration indicating a relationship of the distance between the member to be treated and a plane facing to the member to be treated

of the present invention versus the generating amount of F and CF_2 .

FIG. 5 is an illustration indicating a relationship of the distance between the member to be treated and the plane facing to the member to be treated of the present invention versus the injection ratio of CF_2 /ions,

FIG. 6 is an illustration indicating a relationship between the high frequency (electromagnetic wave) (source) power applied for generating the plasma of the present invention versus the injection ratio of CF_2 /ions onto the member to be treated,

FIG. 7 is an illustration indicating a relationship between the high frequency (electromagnetic wave) (source) power applied for generating the plasma of the present invention versus the ion current density on the member to be treated,

FIG. 8 is two cross sections indicating the shapes before manufacturing and after manufacturing of the oxide film holes on the wafer member to be treated using the present invention,

FIG. 9 is a cross section of another dry etching apparatus using the present invention,

FIG. 10 is a cross section of another dry etching apparatus using the present invention,

FIG. 11 is a cross section of another dry etching apparatus using the present invention,

FIG. 12 is two cross sections indicating the shapes before manufacturing and after manufacturing on the member to be treated using in the present invention,

FIG. 13 is an illustration indicating the dependency of the injection ratio of $\text{CF}_2/(\text{F} + \text{O})$, and the injection ratio of CF_2/ions of the member to be treated on the C_4F_8 gas flow rate using for explanation of the present invention, and

FIG. 14 is an illustration indicating the dependency of the selection ratio at a shoulder portion of the silicon nitride film and the manufacturing shape (taper angle) on the C_4F_8 gas flow rate using for explanation of the present invention.

In accordance with a case when the etching apparatus using the electron-cyclotron resonance (ECR) as indicated in FIG 1 as one of the practical methods for generating the two kinds of electronic temperature regions, the electronic temperature in the ECR region is high (a high electronic temperature region 101), and the low electronic temperature region 102 is formed in another region. An effective ECR region is a region having a magnetic field intensity with a definite width from the magnetic field intensity coinciding with the

ECR condition. That is, the area of the ECR region having a high electronic temperature can be altered by changing the magnetic field gradient. The above status is indicated in FIG. 2. The magnetic field intensity satisfying the ECR condition varies depending on the frequency of the electromagnetic waves. Therefore, the abscissa of FIG. 2 was normalized by a ratio of the magnetic field intensity satisfying the ECR condition to the magnetic field gradient. As indicated in FIG. 2, the high electronic temperature region 201 becomes narrow when the magnetic field gradient of the magnetic field applied externally is increased, and the high electronic temperature region becomes wide when the magnetic field gradient of the magnetic field applied externally is decreased. Accordingly, the generation ratio of CF_2/F can be made variable by controlling the magnetic field gradient in the ECR region. As indicated by the curves 302, 303, and 304 in FIG. 3, the high electronic temperature region is extended by a condition when the magnetic field gradient is small, and the generation ratio of CF_2/F is increased. When the magnetic field gradient is increased, the high electronic temperature region is decreased, and the generation ratio of CF_2/F can be decreased. The curves 301 to 305 in FIG. 3 indicate an example when a gap between an antenna and the wafer is varied. The example will be explained later. When a ratio of

magnetic field gradient/ magnetic field intensity is at least 0.08/cm, change in the generation ratio of CF_2/F becomes small, because the low electronic temperature region becomes dominant. In particular, at least
5 0.15/cm, the generation ratio of CF_2/F is scarcely changed, and controlling the generation ratio of CF_2/F by the magnetic field gradient becomes difficult.

Furthermore, if the magnetic field gradient is constant, the ECR region is approximately inversely
10 proportional to the frequency of the introduced electromagnetic waves. For instance, if the frequency is changed from 2.45 GHz to 450 MHz, the ECR region is extended by three times. Accordingly, the high electronic temperature region can be extended by
15 lowering the frequency of the introduced electromagnetic waves, and the generation ratio of CF_2/F can be increased.

In a case when the magnetic field gradient is fixed (the high electronic temperature region is made
20 definite) by fixing the frequency of the electromagnetic waves, the size of the low electronic temperature region 102 can be altered by changing the distance between the member to be treated 6 and the plane (the antenna 23) facing to the member to be
25 treated. Here, the distance between the member to be treated and the facing plane is called as a gap hereinafter. In FIG. 1, the facing plane is the

antenna 23, but in general, the plane facing to the member to be treated 6 is a portion of the plasma processing chamber 35, and the member to be treated 6 is a plane contacting with the plasma and facing via the plasma. If the magnetic field gradient • magnetic field intensity are fixed at 0.03/cm, and the gap is made broadened, the generating amount of F (the curve 402) is increased as indicated in FIG. 4, because the low electronic temperature region is increased. On the contrary, the generating amount of the CF₂ (the curve 401) is increased with broadening the gap, but decreased if the gap is exceeded 100 mm. The decrement is caused by loss of the once dissociated CF₂ by recombination, because the distance whereby the once generated CF₂ in the ECR region reaches the member to be treated is extended. As explained above, if the gap is broadened, the generation ratio of CF₂/F is decreased. Therefore, the generation ratio of CF₂/F can also be controlled by the gap. The generation ratio of CF₂/F can be controlled in a wide range by controlling both the magnetic field gradient and the gap, simultaneously. Dependency of the generation ratio of CF₂/F on the magnetic field gradient at the gaps of 20 mm, 40 mm, 70 mm, 100 mm, and 120 mm are Indicated in FIG. 3. The abscissa of FIG. 3 indicates the magnetic field gradient divided by the ECR magnetic field intensity, and each of the marks 301 to 305

corresponds to the gap from 20 mm to 120 mm, respectively.

The generation ratio of CF_2/F becomes constant at the low magnetic field gradient side (equal to or less than 0.05/cm) of the gap of 20 mm (the curve 301), because the space in the gap becomes only the high electronic temperature region. When the gap exceeds 100 mm, the generation ratio of CF_2/F becomes not to be dependent on the magnetic field gradient, because the fluorocarbon is dissociated completely as indicated by the curve 305. When the gap is 20 mm, the plasma space is too narrow, and a pressure difference is generated at the central portion from the peripheral portion of the member to be treated. That means, the pressure on the member to be treated is fluctuated, and an uniform manufacturing becomes difficult.

In oxide film etching process, not only the generation ratio of CF_2/F , but also the injecting amount of CF_2 Which becomes an etching protecting film against ion spattering, and the injecting amount of ions which generate ion spattering must be controlled, in order to obtain the selectivity for the resist film and the silicon nitride film. Dependency of the injection ratio of CF_2 /ions to the member to be treated on the magnetic field gradient at the gap of 50 mm is indicated in FIG. 5. When the magnetic field gradient is increased, the high electronic temperature

region is decreased, and the injection ratio of CF_2/ions is slightly decreased. The curve 501 indicates that the injection ratio of CF_2/ions can be controlled in the range of approximately 35 % by the magnetic field gradient. When the magnetic field gradient is increased, the generating amount of CF_2 is decreased. In a case of large magnetic field gradient, the magnetic lines of force become divergent. However, the ions generated in the high electronic temperature region move along the magnetic lines of force, and the number of the ions, which are not injected into the member to be treated but escape around the member to be treated, is increased. Therefore, a large difference can not be observed in the injection ratio of CF_2/ions .

The generating amount of CF depends not only on the electronic temperature and the electronic density, but also on the gas flow rate of the fluorocarbon gas. In a case when the gas flow rate is 10 ml/min (the curve 601) as indicated in FIG. 6, the injection ratio of CF_2/ions on the member to be treated is saturated at approximately 8, but with 20 ml/min (the curve 602) or 30 ml/min (the curve 603), the saturated value of the injection ratio of CF_2/ions becomes approximately 16 or 23, respectively. Because the ion current density does not depend on the gas flow rate, the generating amount of CF_2 can be controlled by the gas flow rate, and the ion current density can be controlled by the high

frequency power. Therefore, the injection ratio of CF_2/ions can be set in accordance with the process . For instance, in accordance with FIG 6, the injection ratio of CF_2/ions can be varied approximately from 8 to 20 by altering the gas flow rate in the range of 10-30 ml/min with the high frequency power of 1000 w. Accordingly, the injection ratio of CF_2/ions can be controlled in a wide range by controlling with a combination of the magnetic field gradient and the gas flow rate. The electronic density in plasma is approximately proportional to the high frequency power (this is an input power from a high frequency power source generating electromagnetic waves, but simply called as high frequency power, here), and the injection amount of the ions on the member to be treated (ion current density) is also proportional to the high frequency power. As indicated by the curve 701 in FIG. 7, the ion current density is increased approximately in proportional to the high frequency power. The etching velocity of the oxide film is approximately proportional to the ion current density. Therefore, in order to perform a quick etching, an ion current of at least 5 mA/cm^2 is necessary. Furthermore, as described previously, the ion current density is decreased by broadening the gap. Therefore, the high frequency power must be increased, in order to obtain the same ion current density as before when the gap is

broadened.

As explained above in a case of the ECR etching apparatus, the generation ratio of CF_2/F can be controlled independently from the generating amount of the ions by controlling the position of the ECR, magnetic field gradient, frequency of introduced electromagnetic wave, distance between the member to be treated and a plane facing to the member to be treated, and gas flow rate.

In manufacturing the gate electrode and the metallic circuit, generation of Cl radicals and Br radicals can be suppressed by controlling the two electronic temperature regions. The dissociation of Cl_2 to Cl requires a dissociation energy of 2.5 eV, and the dissociation of HBr to Br requires a dissociation energy of 3.8 eV. Accordingly, the generating amount of Cl radicals and Br radicals can be suppressed in the low electronic temperature region having an electronic temperature lower than the dissociation energy, because generating amount of the radicals is small and recombination of the radicals is generated.

In accordance with decreasing the generating amount of Cl and Br, side etching at side planes of the gate electrode and the metallic circuit can be suppressed. The ions are generated mainly in the high electronic temperature region, and the generating amount of the ions can be controlled independently from

Cl and Br.

Hitherto, the oxide film etching method has been explained particularly among the manufacturing methods of the member to be treated on the semiconductor device by dry etching. However, the etching method of the present invention can be applied not only to manufacturing the semiconductor device, but also to fine manufacturing using dry etching apparatus for liquid crystal TFT, DVD disk, DVD head, magnetic head, and so on.

The embodiment using the apparatus indicated in FIG. 1 is explained in details, hereinafter. The apparatus comprises an etching treatment chamber 1 composed of a vacuum chamber 30, which is an external cylinder of the process chamber itself, and an internal cylinder 22. The internal of the etching treatment chamber 1 comprises a plasma treating chamber 35, an antenna 23, an antenna dielectric body 28, and a treating plate 5. An etching gas (treating gas) is introduced into the plasma treating chamber 35 through an gas inlet 24 provided at the antenna 23, and plasma is generated by introducing electromagnetic waves of 300 MHZ to 600 MHZ generated by a high frequency power source 17 via a matching box 18 through the antenna 23 into the plasma treating chamber 35. As the etching gas, CF group gas is preferably used for the etching of insulating film such as silicon oxide film and the

like. In order to propagate the electromagnetic waves to the plasma treating chamber 35 effectively, an outer diameter of the antenna 23 and size and material of the antenna dielectric body 28 are determined so as to make
5 the electromagnetic waves resonate between the antenna 23 and an antenna earth 29 with a desired mode (here, TM01). The electromagnetic waves resonate between the antenna 23 and the antenna earth 29, and the electromagnetic waves are propagated to the plasma
10 treating chamber 35 via peripheral portions of the antenna dielectric 28. In order to discharge effectively, three solenoid coils 4 for generating magnetic field contained in a coil case 30, respectively, are arranged in yoke 21 at peripheral
15 portion of the etching treatment chamber, and a coil current is set in order to form a magnetic field between 0 to 320 Gauss at approximately above the process platform. Then, high density plasma having an electronic density of at least 10^{11} electrons/cm³ is
20 generated using electron-cyclotron resonance. The process platform 5 are provided in the plasma treating chamber 35. A member to be treated 6 is placed on the process platform, and etched with the gas plasma. The member to be treated 6 is transferred into the etching
25 treatment chamber 1 through a valve 16. The etching gas is introduced into the plasma treating chamber 35 through a gas flow controller 10 and a valve 9, and

exhausted outside the plasma treating chamber 35 through an exhaust valve 8 by an exhaust pump 7. The pressure in the plasma treating chamber 35 is controlled to be a designated value by a conductance valve 8 provided on the top of the exhaust pump 7. An inner cylinder 22 is arranged on the side wall of the plasma treating chamber 35, in order to control accumulation of reaction products and to save clean up operation time by changing components at clean up operation. The process platform 5, whereon the member to be treated (the member to be treated 6 in the embodiment of the present invention is a wafer, then, the member to be treated and the wafer are used in the same meaning) is placed, is provided with a high frequency power source 12 and a matching box 11, which can supply high frequency bias from 400 KHz to 13.56 MHZ to the electrode 27. The position of the process platform 5 can be set with a distance in the range of 20 mm to 150 mm from the antenna 23. The periphery of the process platform 5 has a structure, wherein a focus ring 25 having a width of approximately 30 nun can be arranged surrounding the wafer, and the high frequency waves applied to the wafer 6 are partly, approximately 10 % to 20 %, applied to the focus ring 25 by branching with a condenser 26 (it may not be an electronic component, but it may be formed by forming a dielectric film and the like on surface of the high

frequency bias applying portion 27) . The mark 14 indicates a susceptor. The material of the focus ring 25 is single crystal silicon, and impurity doped Si or SiC can be provided. The susceptor 14 composed of
 5 insulating material such as alumina and the like is arranged at periphery of the focus ring 25 and the high frequency bias applying portion 27 for preventing wafer bias from leaking to periphery, and preventing the high frequency bias applying portion 27 from being
 10 damaged by plasma. A high frequency power source 20 is connected to the antenna 23 via a high frequency filter 19 provided with a stab tuner 18 and a filter circuit, in order to apply high frequency having different frequency (10 KHz to 27 MHz) from the high frequency
 15 power source to supply electromagnetic waves to the antenna 23 . The material of the antenna 23 is impurity doped Si at the plasma treating chamber side, and Al at its opposite side.

As the member to be treated 6 eight inches silicon
 20 wafer having the structure indicated in FIG. 8 formed on its surface is transferred from an adjacent transfer chamber (not shown in the figure) via a gate valve 16. The wafer 88 before etching is composed of a silicon wafer 87 having a gate oxide film 86 of 4nm thick
 25 formed thereon, and gate electrodes 85 of 300 nm thick and 80 nm wide composed of polycrystalline Si and W formed on a part of the surface of the gate oxide film.

Silicon nitride film 84 of 200 nm thick is formed on the upper surface of the gate electrode, and silicon nitride film 84 of 60 nm thick is formed on the side surface of the gate electrode and the upper surface of the gate oxide film so as to cover the gate electrode 5 85. An oxide film 83 (SOG and CVD oxide film) of 1600 nm thick (at the most thick portion) is formed on the upper surface of the silicon nitride film. Above the film, a reflection preventing film 82 of 80 nm thick 10 and a resist mask 81, whereon a hole pattern of 130 nm in diameter is exposed and developed, of 500 nm thick are formed. The width of the oxide film 83 existing between the gate electrode is approximately 60 nm.

In accordance with FIG. 1, a mixed gas consisting 15 of Ar 800 ml/min, C_5F_8 20 ml/min, and O_2 20 ml/min, is introduced into the plasma treating chamber 35 through the gas inlet 24, and pressure of the gas is maintained at 2.5 pa. Gas plasma is generated by applying electromagnetic waves of 450 MHz, 1.3 kW, and the oxide 20 film is etched by applying bias of 2 MHz, 1000 W to the process platform 5. The height of the process platform is adjusted so as to make the distance (gap) from the wafer surface to the antenna 23, which is the facing plane to the wafer, to be 50 mm. The coil current is 25 adjusted to make the magnetic field intensity 160 Gauss at a position far from the wafer 6 by 35 mm on the central portion of the wafer and a position far from

the wafer 6 by 50 mm at the surrounding of the wafer,
and to make the magnetic field gradient 12 gauss/cm at
the same positions (ECR height). The magnetic field
intensity of 160 gauss is a magnetic field intensity to
5 satisfy the ECR condition, because the frequency of the
electromagnetic waves applied to the antenna 23 was set
as 450 MHz in the present embodiment. Under the above
condition, the thickness of the ECR region is
approximately 17 mm, and the region can be regarded as
10 the high electronic temperature region 101. The
electronic temperature is approximately 8 eV.
Furthermore, high frequency bias of 13.56 MHz is
applied to the antenna 23 by 300 W. The electronic
temperature in the low electronic temperature region
15 102 corresponding to the region other than the ECR
region is approximately 2 eV. The generation ratio of
 CF_2/F by dissociation of C_5F_8 becomes approximately
1.5. However, the injecting amount of F into the wafer
6 is actually decreased by a reaction with the polymer
20 (organic group accumulated compounds such as etching
gas, reaction products, and so on) on the surface of
the antenna 23 corresponding to the plane facing to the
wafer, and consumption of F by Si on the surface of the
antenna 23 with applied bias from the high frequency
25 power source 20 to the antenna 23. Therefore, the
injection ratio of CF_2/F into the wafer becomes
approximately 12. As explained above, the high

electronic temperature region 101 corresponding to the ECR region, and the low electronic temperature region 102 are formed by setting the gap between the wafer 6 and the antenna 23, the ECR height, and the magnetic field gradient. As the result, the CF_2/F ratio corresponding to two kinds of electronic temperature regions could be obtained. Naturally, the CF_2/F ratio is readily variable by controlling the current value of the coil 4 to change the magnetic field gradient. The injection ratio of CF_2 /ions into the wafer 6 is readily variable by controlling the input power of the electromagnetic waves, that is, the power from the high frequency power source 20, because the ion current can be changed readily by controlling the power. In accordance with the present embodiment, a method to consume F with the surface of the antenna 23 composed of Si by applying high frequency bias having a frequency different from the electromagnetic waves of 450 MHz from the high frequency power source 20 to the antenna 23 in order to control the CF_2/F ratio has been indicated. However, it is needless to say that the above method is not necessarily the substantial method for controlling the CF_2/F ratio.

The CF_2/F ratio has been set by the above method. However, unnecessary C from C_5F_8 is injected into the wafer in a form of C_2 or C radicals. Consequently, an accumulated film composed of C is formed on the surface

of the wafer 6, and the film disturbs proceeding the etching. Accordingly, it becomes necessary to add O_2 in order to eliminate the accumulated film in the present process.

5 Main etching conditions can be determined by the above setting. Next, if the input power of the electromagnetic waves is assumed to be 1000 W, the ion current density becomes approximately 5 mA/cm². Under the above condition, the oxide film hole of 100 nm in
10 diameter was etched. Then, the etching velocity of 500 nm/min, and the selection ratio of 8 to the resist were obtained.

Next the oxide film etching was performed on a self-align contact (SAC) structure indicated in FIG. 8.
15 FIG. 8 on the left side indicates a cross section of the wafer before etching, and FIG. 8 on the right side indicates a cross section of the wafer after etching. The result is indicated as the shape 89 after etching. After starting the etching, the silicon nitride film
20 begins to be appeared after approximately 145 seconds.

Subsequently, the etching process is finished after approximately 200 seconds. Generally, the shoulder portion 84a (at a corner portion of either right or left upper portion of the gate electrode) of
25 the silicon nitride film 84 is readily reduced and increasing the selection ratio at the shoulder portion 84a of the silicon nitride film 84 and the oxide film

83 is extremely difficult. However, in accordance with the condition of the present embodiment, a relatively high value, such as approximately 20, was obtained for the selection ratio of the reduction at the shoulder
5 portion 84a of the silicon nitride film 84.

How etching characteristics may change when the CF_2/F ratio has been altered is as follows:

For instance, in a case when the magnetic field gradient is 4 Gauss/cm, the resist selectivity is very
10 high, the silicon nitride film is hardly reduced, and extremely high selection ratio can be obtained. However, the etching process is terminated after approximately 145 seconds due to the lack of F. The selection ratio can be controlled by adjusting the
15 magnetic field gradient as explained above, but in order to perform the etching process practically, it is necessary to set an optimum condition.

In order to utilize the etching method of the present invention more effectively, changing the
20 magnetic field gradient in the middle of the etching process is effective. The etching process is proceeded with the magnetic field gradient of 4 Gauss/cm, which makes it possible to take a large selection ratio, during 170 seconds from the starting point of the
25 etching process; after 170 seconds to 190 seconds, the magnetic field gradient is adjusted to 8 Gauss/cm, which makes it possible to maintain the etching

process and to ensure the somewhat desirable selection ratio; and after 190 seconds to 200 seconds the magnetic field gradient is adjusted to 12 Gauss/cm, which makes it possible to proceed the etching to the bottom of the SAC holes. In the above case, the reducing amount of the silicon nitride film 84 can be suppressed at minimum, and the selection ratio to the shoulder portion of the silicon nitride film can be approximately 30.

10 The embodiment, wherein the magnetic field gradient is altered in the middle of the etching process for controlling the high electronic temperature region 101 and the low electronic temperature region 102 in order to optimize the CF_2/F ratio, has been indicated above. However, the substantial point of the present invention is in optimizing the CF_2/F ratio during the etching process. That means, instead of adjusting the magnetic field gradient, the ECR height may be changed. The gas, gas flow rate, and input power of the electromagnetic waves are similar. The adjusting range of the magnetic field gradient is restricted by an arrangement of the coil 4, and a range of the current. However, when the ECR magnetic field intensity of 160 Gauss in a case when 450 MHz is introduced into the antenna 23 is taken as a standard, the adjusting range may be the range from 1.6 Gauss/cm to 24 Gauss/cm. That is, the magnetic field

gradient/ECR magnetic field gradient is taken in the range from 0.15 /cm to 0.01 /cm.

Next, how the etching characteristics is changed with variation in injecting amount of F into the wafer, that is the member to be treated 6, will be explained, and the importance of controlling CF_2 , F by the present invention will be indicated.

The etching characteristics was studied, in a case when the gap and the ECR height were maintained at constant, and the magnetic field gradient was fixed at 8 Gauss/cm; under the above condition, the amount of F was changed by applying a bias to the antenna 23 for controlling the reaction of F with Si at the surface of the antenna. When the power of the high frequency power source 20 is decreased from 300 W to 200 W in order to change the bias applied to the antenna 23, the consuming amount of F at the antenna is decreased. As the result, the reaching depth in the hole manufacturing becomes as same as the case of 12 Gauss/cm, and the selection ratio to the shoulder portion of the silicon nitride film becomes approximately 20. Furthermore, when the power of the high frequency power source 20 is changed to 100 W, the reaching depth of the hole becomes deeper, but a sufficient shoulder selection ratio can not be obtained. If the power of the high frequency power source 20 is further decreased, accumulated materials

are adhered onto the surface of the antenna, and stable etching process becomes difficult. In accordance with the above result, it is revealed that the reaching depth of the etching hole becomes deeper by increasing the CF_2/F ratio, but the selection ratio of the silicon nitride and the oxide film is decreased. On the contrary, when the CF_2/F ratio is decreased, that is, in a case when F is decreased, improvement in the selection ratio can be expected. If the power of the high frequency power source 20 is increased to 800 W, the consumption of F is further increased, the resist selection ratio is increased, and the selection ratio of the silicon nitride film is increased to approximately 30, but etching residue is generated. In order to solve the above problem, the power of the high frequency power source 20 is maintained at 800 W, and the flow rate of O_2 is changed to 23 ml/min. Then, the etching residue is eliminated, but the selection ratio of the silicon nitride film is decreased to approximately 23. If the power of the high frequency power source 20 is further increased, a consuming effect of F can be observed. However, when the power exceeds 1000 W, the reaction at the surface of the antenna becomes active, and the reaction products are adhered to the surface of the wafer as the etching residue. Accordingly, setting the CF_2/F ratio in an appropriate range is important to ensure the desirable

etching depth and the selection ratio.

Next, effects of the gap on the etching characteristics are indicated.

Under the etching condition described above, the
5 power of the high frequency power source 20 is
maintained at 300 W, and the magnetic field gradient is
set at 4 Gauss/cm, and the gap is broadened from 50 mm
to 90 mm. Then, on the contrary to the case of gap of
50 mm, wherein the sufficient etching depth could not
10 be obtained due to the lack of F, the problem of
etching stop was solved, because F was increased with
increasing the high electronic temperature region 101
by decreasing the magnetic field gradient, and
increasing the low electronic temperature region 102 by
15 broadening the gap. The selection ratio at the
shoulder portion of the silicon nitride film in the
above case was approximately 20.

Furthermore, when the gap is broadened to exceed
100 mm, C_5F_8 is dissociated excessively, and C, F
20 radicals become excess. Therefore, the etching stop is
generated, and sufficient selectivity can not be
obtained, even if radical control is performed with the
magnetic field gradient. On the contrary, when the gap
is shortened to less than 30 mm, the gap becomes as
25 almost same as the ECR region, and only the high
electronic temperature region 101 is formed.
Therefore, the dissociation control by the magnetic

field gradient becomes difficult. Furthermore, the gas supplied from the gas inlet 24 flows through a narrow space between the wafer 6 and the antenna 23.

Therefore, a pressure distribution is generated on the surface of the wafer, and uniform manufacturing becomes difficult. As described above, the areas of the high electronic temperature region 101 and the low electronic temperature region 102 can be altered by setting the gap between the wafer 6 and the antenna 23 in the range of 30 mm to 100 mm, and as the result, adjustment of the CF_2/F ratio becomes possible. In accordance with the present embodiment, the gap between the wafer 6 and the antenna 23 was explained, but the gap between the wafer 6 and the plane facing to the wafer is similar and the gap is not restricted to between the antenna and the wafer. Next an adequate pressure range in the present invention is explained. Generally, if the pressure is low, the energy obtained by an electron, during being accelerated by electromagnetic waves until collided with other gas molecule, becomes large. That is, the electronic temperature tends to be high. Physical meaning of the present invention lies in controlling the electronic temperature and its region, and controlling the dissociation of gas molecules. Therefore, the pressure range has an important meaning. However, because the dissociation energy of gas molecule differs depending

on the kind of the gas molecule, the adequate electronic temperature and pressure range differ depending on the kind of the etching gas.

When Ar gas flow rate is set as 400 ml/min and gas pressure is set as 0.1 Pa, the electronic temperature in the low electronic temperature region 102 becomes high as 2.8 eV. When etching treatment is performed under the condition of oxygen flow rate 5 ml/min, gap 50 mm, and magnetic field gradient 4 Gauss/cm, the selection ratio at the shoulder portion of the silicon nitride is approximately 18. Furthermore, when the gas pressure is decreased to lower than 0.1 Pa, the electronic temperature in the low electronic temperature region 102 is increased rapidly, and control of the CF_2/F ratio by the magnetic field gradient becomes difficult. When influence of the gas pressure is studied in view of the resist selection ratio, it is revealed that the resist selection ratio is approximately 8 with the gas pressure in the range from 2.5 Pa to 1.5 Pa, but the resist selection ratio is decreased to approximately 6 at the gas pressure of 0.5 Pa, and the resist selection ratio is decreased to approximately 5 when the gas pressure is decreased to 0.1 Pa. Based on necessity to keep the selection ratio high, the gas pressure must be at least 0.1 Pa. In accordance with the above reason, the lower limit of the gas pressure is approximately 0.1 Pa, when the

etching process is performed with CF group gas. When the gas pressure is set at 4 Pa, retention time of the gas becomes longer in comparison with a case of lower pressure, and injection amount of the reaction products into the wafer 6 is increased. Therefore, accumulative adhered substance tends to be formed on the surface of the wafer 6, and under the condition of magnetic field gradient 12 Gauss/cm, gap 50 nun, power of the high frequency power source 20 of 300 W, the etching residue is generated at the bottom of the hole. The etching residue was disappeared by decreasing the power of the high frequency power source 20 from 300 W to 150 W to suppress the consuming amount of F, in order to eliminate the accumulative adhered substance with F.

15 When the gas pressure is further increased to 6 Pa, the gas retention time is extended, and the etching residue is readily generated. However, if Ar flow rate is increased to 1200 ml/min, the gas retention time becomes as same as the case of 4 Pa, and similar etching depth can be obtained. If the gas pressure is further increased, slant injection of the ions are increased, and obtaining perpendicularly manufactured shapes becomes difficult. Furthermore, control of plasma composition becomes difficult due to

20 dissociation of the reaction product (mainly, reaction product of the resist), even if the generation ratio of CF_2/F in the etching gas is controlled by the magnetic

field gradient. Because of the reason described above, the upper limit of gas pressure in the etching process with the CF group gas is 4 Pa. Influence of the gas pressure when the manufacturing dimension becomes more precise was further studied. The hole diameter of 130 nm, from which the above results have been obtained, is decreased to 100 nm. Then obtaining a sufficient etching velocity in the hole becomes difficult with 4 Pa, even if the oxygen flow rate is increased.

However, if the gas pressure is decreased to equal to or lower than 3 Pa the similar etching process with the case of the hole diameter of 130 nm becomes possible. In a case when the hole diameter is further small as 80 nm, the gas pressure may further be decreased to equal to or lower than 25 Pa. As explained above, it has been revealed that decreasing the gas pressure is an effective countermeasure to correspond to increasing preciseness of the manufacturing dimension. The pressure range of the present invention from the lower pressure limit of 0.1 Pa to the upper pressure limit of 4 Pa can sufficiently correspond to the requirement. As described above, the CF_2/F ratio can be varied by controlling the magnetic field gradient even if the ion current is maintained at a definite value. By decreasing the magnetic field gradient, the selection ratio to the resist can be increased. However, decreasing the magnetic field gradient means decreasing

difference of the magnetic intensity at various portions, and also means forming an uniform magnetic field in the etching apparatus. In order to realize the above condition, it is necessary to provide many
5 coils around the etching apparatus. If the magnetic field intensity to satisfy the ECR condition is decreased, the magnetic field gradient to satisfy effectively the ECR condition is decreased in proportional to the magnetic field intensity, and the
10 magnetic field gradient can readily be controlled. Because the magnetic field intensity to satisfy the ECR condition is determined by the frequency of the electromagnetic waves for generating plasma, lowering the frequency of the electromagnetic waves is
15 advantageous in coil designing and cost down of the apparatus. In accordance with the present embodiment, the frequency of the electromagnetic waves was taken in the range of 300 MHZ to 600 MHZ in consideration of easiness of plasma start, the electronic temperature of
20 the plasma generated in the ECR region, and others, in addition to the above features.

In accordance with the above embodiments, the cases of $\text{Ar}/\text{C}_5\text{F}_8/\text{O}_2$ as the etching gas are indicated. However, even if any one of the CF group gases such as
25 C_4F_8 , C_4F_6 , C_3F_6 , and C_3F_8 is used as the etching gas, approximately the similar result can be obtained, except the optimum flow rate of oxygen. Approximately

similar result can be obtained, even if any one of SF_6 , CF_4 , and SiF is used instead of oxygen. Furthermore the selectivity to the resist can be increased by addition of any one of SiH_2F_2 , SiH_4 , and CO gas.

5 The similar result can be obtained by using the high frequency bias applied to the antenna 23 for controlling F by branching from the high frequency power source 12, which applies the bias to the wafer 6. When branching, it is effective if phases of the high
10 frequency bias applied to the antenna 23 are shifted by approximately 90 degrees from the phases of the high frequency bias applied to the wafer 6. If any insulating film such as glass materials containing boron, or phosphorus (BPSG, PSG) , silicon glass
15 containing organic substance (organic SOG) , and oxide film containing F, is used as the material for the oxide film, i.e. the film to be etched, the similar results can be obtained.

Next, another embodiment using the apparatus
20 indicated in FIG. 1 is explained.

Eight inches silicon wafer is transferred into the apparatus as the member to be treated. On the silicon wafer, a silicon nitride film of $0.1 \mu\text{m}$ thick is formed, an oxide film of $1.5 \mu\text{m}$ thick is formed
25 thereon, and a resist mask reprinted with a mask pattern is formed thereon. Holes having 150 nm In diameter are formed on the resist mask.

In accordance with the apparatus indicated in FIG. 1, a mixed gas consisting of Ar 200 ml/min, and C_4F_8 10 ml/min is introduced into the plasma treating chamber 35 through the gas inlet 24, and pressure of the gas is maintained at 1 Pa. Gas plasma is generated by applying electromagnetic waves of 450 MHz, 1 kW, and the oxide film is etched by applying bias of 800 KHz, 800 W to the process platform 5. The process platform is positioned by 60 mm from the antenna 23, and the coil current is adjusted to make the magnetic field intensity 160 Gauss at a position above the wafer 6 by 40 mm, and to make the magnetic field gradient 4 Gauss/cm at the same positions (ECR height). Under the above condition, the thickness of the ECR region is approximately 35 mm, which can be regarded as the high electronic temperature region 101, and the electronic temperature is approximately 8 eV. The electronic temperature in the low electronic temperature region 102 corresponding to the region other than the ECR region is approximately 2 eV. The generation ratio of CF_2/F by dissociation of C_4F_8 becomes approximately 1.0. However, the actual injecting amount of F into the wafer 6 is further decreased by consumption on the surface of the antenna 23. Therefore, the injection ratio of CF_2/F into the wafer becomes approximately 3. The ion current density becomes approximately 5 mA/cm². Under the above condition, the etching velocity of the

oxide film is approximately 500 nm/min, selection ratio to the resist is 20, and the selection ratio to the nitride film of substrate is 30.

How deep the etching process can be performed was studied by increasing the thickness of the oxide film to 3 μm , maintaining the contact hole diameter as 150 nm. As the result, the etching process was terminated at the depth of 2 μm . In accordance with the prior art, termination of the etching process in this case must be prevented by adding oxygen gas, in order to eliminate the accumulated substance at the bottom of the hole. However, when the oxygen is added, the selection ratio of the resist is decreased to approximately 5. On the contrary, in accordance with the present invention, if the generation amount of F is increased by increasing the magnetic field gradient from 4 Gauss/cm to 10 Gauss/cm, the etching process for the oxide film of 3 μm thick and the contact hole of 150 nm in diameter is not terminated at middle of the process, and approximately perpendicularly manufactured shape can be obtained. In this case, the selection ratio to the resist is decreased to approximately 10, but the selection ratio is larger in comparison with the case of oxygen addition.

As explained above, corresponding to various etching conditions becomes easy by changing the magnetic field gradient for controlling the CF_2/F

ratio, even if the gas condition is same, and the addition of oxygen and the like becomes unnecessary.

Another embodiment wherein the additive gas becomes unnecessary is indicated, hereinafter.

5 Under the same etching conditions such as the frequency of the electromagnetic waves applied to the antenna 23 is 450 MHz and the magnetic field gradient is 4 Gauss/cm, the distance between the wafer 6 and the antenna 23 is changed from 60 mm to 100 mm, and
10 manufacturing the patterned contact hole of 150 nm in diameter is performed on a silicon oxide film of 1.5 μm thick. The relative injection amount of F into the wafer 6 is increased by broadening the gap, because the low electronic temperature region 102 is increased and
15 the influence of F consumption at the surface of the antenna 23 is decreased. Therefore, the selection ratios to the resist and the nitride film are decreased to 10 and 12, respectively. When the gap was equal to or more than 100 mm, any influence to the selection
20 ratio was not observed. In addition to the above condition, if CH_2F_2 gas is added by approximately 5 ml/min, the selection ratio to the resist becomes 20, and the selection ratio to the nitride film becomes approximately 25. However, CH_2F_2 is a strongly
25 accumulative, and adhered onto the inner wall. Therefore, frequency of cleaning is increased, and throughput is decreased. That is, decreasing the gap

in order to improve the selection ratio is more advantageous in view of the throughput. However, if the gap is decreased to 40 mm, the injection amount of F is decreased, and the etching process is terminated at the
5 depth of approximately 1.2 μm , even the selection ratio is increased. As explained above, the desired etching characteristics can be obtained by controlling the CF_2/F ratio with controlling the distance between the wafer 6 and the antenna 23, and the magnetic field
10 gradient, without adding any gas. If oxygen is added, sufficiently satisfying etching characteristics can be obtained even if the gap is decreased to 30 mm.

Next, another embodiment using the apparatus indicated in FIG. 10 is explained. The same numeral
15 marks are designated to the same component in FIG. 10 as the components indicated in FIG. 1, and explanation is omitted. In accordance with the present apparatus, an etching gas is introduced into the plasma treating chamber 35; which is composed of a vacuum vessel 13,
20 i.e. an external cylinder, and an inner cylinder 22; through the gas inlet 66, high frequency waves in the range of 10 MHz to 100 MHz are generated by a first high frequency power source 61 and a second high frequency power source 62, and gas plasma is generated
25 by introducing the high frequency waves into the plasma treating chamber 35 through ring antennas 63, 64, and a wafer facing plane 65 composed of ceramic material.

Each of matching boxes 67, 68, is provided to
respective of the high frequency power sources 61, 62,
in order to supply power effectively to the plasma.
The plasma becomes high density plasma having an
5 electron density of at least 10^{11} electrons/cm³. The
process platform 5 is provided in the plasma treating
chamber 35, and the member to be treated 6 (wafer) is
placed on the process platform and etched with gas
plasma. The etching gas is introduced into the plasma
10 treating chamber 35 through the gas flow rate
controller 10 and the valve 9, and exhausted outside
the etching treatment chamber 1 by the exhaust pump 7.
The process platform 5, whereon the member to be
treated 6 is placed, is provided with the high
15 frequency power source 12 and matching box 11, and
high frequency bias from 400 KHz to 13.56 MHz can be
applied. The wafer facing plane 65 is made of a
ceramic material composed of Si 50 % and SiC 50%. An
elevator is provided to the process platform 5, in
20 order to make it possible to adjust the distance
between the wafer 6 and the wafer facing plane 65 in
the range from 20 mm to 150 mm. Desirably, the
distance between the process platform 5 and the wafer
facing plane 65 in the range from 30 mm to 100 mm is
25 adoptable. The same numeral marks are designated to
the same component having the same function in FIG. 10
as the components indicated in FIG. 1, and explanation

in details is omitted.

Eight inches silicon wafer is transferred into the apparatus as the member to be treated. On the silicon wafer, an oxide film of 2 μm thick is formed, and a
5 resist mask reprinted with a mask pattern is formed thereon. Holes having 200 nm in diameter are formed on the resist mask.

In accordance with the apparatus, a mixed gas consisting of Ar 30 ml/min, and C_3F_8 20 ml/min, H_2 8
10 ml/min is introduced into the etching treatment chamber 1 through the gas inlet 24, and pressure of the gas is maintained at 0.7 Pa. The process platform 5 is adjusted so that the distance from the wafer 6 to the wafer facing plane 65 becomes 70 mm. Gas plasma is
15 generated by applying high frequency waves of 13,56 MHz, 1500W, to the first ring antenna 63, and high frequency waves of 13,56 MHz, 1000W, to the second ring antenna 64, and the oxide film is etched by applying bias of 800 KHz, 1200 W to the process
20 platform 5. Under the above condition, the electronic temperature around the first ring antenna 63 is approximately 10 eV, and the electronic temperature around the wafer is approximately 4 eV. The etching velocity of the oxide film is approximately 700 nm/min,
25 and the selection ratio to the resist becomes approximately 25. However, the etching termination can be observed at the middle of the contact holes.

then, the high frequency power applied to the second ring antenna 64 is altered to 500 W, and the frequency is changed to 100 MHz. The electronic temperature around the wafer is decreased to
5 approximately 2 eV. because the plasma density is mainly determined by the first ring antenna 63, wherein the high power is introduced, the ion current density is not changed, and the etching velocity of the oxide film is approximately 700 nm/min, but the selection
10 ratio to the resist is decreased to approximately 10 by lowering the electronic temperature. However, under this condition, the etching termination is not generated.

If the high frequency power to be applied to the
15 second ring antenna 64 is changed from 1000 W to 500 W in accordance with elapsing the etching time at a constant frequency of 100 MHz, the etching process is not terminated, the contact holes are formed, and average selection ratio to the resist during the
20 etching process becomes approximately 20.

The pressure of the gas introduced in the plasma treating chamber 35 is as same as the previous embodiment, such as the range from 0.1 Pa to 4 Pa is adoptable.

25 As explained above, even in accordance with the induction coil type plasma, not the ECR type, the electronic temperature in the plasma treating chamber

can be controlled by providing plural induction coils and controlling the frequency and the power of the high frequency waves applied to each of the induction coils. By performing the dissociation control of CF group gas

5 with the method explained above, the etching process satisfying the etching depth and the selection ratio becomes available. Substantially, the present method is also based on the same principle as the ECR method, and the operations such as adjustment of the gap and the

10 like are similar. If the wafer facing plane is composed of a dielectric material reactive with the etching gas (single crystal Si, quartz, alumina, and the like), a reaction is generated at its surface, and control of etching species becomes possible as stated

15 previously. Because the present apparatus is induction combination type, electrical conductive materials (Si or SiC doped with Aluminum, P, B, and so on) can be used for composing the wafer facing plane. The apparatus structure indicated in FIG. 9 is

20 substantially similar with the apparatus indicated in FIG. 10. The apparatus indicated in FIG. 9 comprises somewhat slanted side wall, different from the apparatus indicated in FIG. 10 wherein two sets of antennas are provided on the wafer facing planes, and

25 two sets of antennas 63, 64 are provided on the side wall. The present apparatus differs from the apparatus in FIG. 10 only in the location of the antennas, and

operation and advantages of the present invention are similar. The same advantages can be obtained, even if the etching chamber is made cylindrical shape as indicated in FIG. 10, and the antennas are provided on
5 the side wall portion. In accordance with the apparatus indicated in FIG. 9, the components designated by the same numerical marks as FIG. 1 and FIG. 10 have the same functions (the exhaust system is omitted), and explanation in details is omitted.

10 Another embodiment using the apparatus indicated in FIG. 11 is explained, hereinafter.

In accordance with the present apparatus, plasma treating chamber 35, atmospheric antenna 34, antenna dielectric 28, quartz 33, dielectric having a gas
15 inlet 13, and process platform are provided in the etching treatment chamber 1. An etching gas is introduced into the plasma treating chamber 35 via the gas inlet of the dielectric 13, and gas plasma is generated by introducing the electromagnetic waves of
20 300 MHz to 600 MHz generated by the high frequency power source 17 into the plasma treating chamber 35 via the matching box 18 and the atmospheric antenna 34. In order to make the electromagnetic waves be propagated effectively to the plasma treating chamber
25 35, the outer diameter of the antenna 34, and size and material of the antenna dielectric 28 are determined so as to make the electromagnetic waves cause a resonance

with a desired mode (here, TMOI) between the atmospheric antenna 34 and the antenna earth 29. The electromagnetic waves cause a resonance between the antenna 34 and the antenna earth 29, and are propagated to the plasma treating chamber 35 via the quartz plate 33 through the peripheral portion of the antenna dielectric 28. In order to discharge effectively, three solenoid coils 4 for generating magnetic field contained in a coil case 30 , respectively, are arranged at peripheral portion of the etching treatment chamber, and a coil current is set in order to form a magnetic field between 0 to 320 Gauss at approximately above the process platform 5. Then, high density plasma having an electronic density of at least 10^{11} electrons/cm³ is generated using electron-cyclotron resonance. The process platform 5 is provided in the plasma treating chamber 35. A member to be treated 6 is placed on the process platform 5, and etched with the gas plasma. The etching gas is introduced into the etching treatment chamber 1 through the gas flow controller 10 and the valve 9, and exhausted outside the etching treatment chamber 1 by the exhaust pump 7. The pressure in the plasma treating chamber 35 is controlled to be a designated value by a conductance valve 8 provided on the top of the exhaust pump 7. The process platform 5, whereon the wafer is placed, is provided with the high frequency power source 12 and

the matching box 11, which can supply high frequency bias from 400 KHz to 13.56 MHz. An inner cylinder made of quartz 22 is arranged at the side wall portion of the plasma treating chamber 35, and an earth 2 is
5 provided concurrently for supporting the inner cylinder 22.

As the member to be treated, eight inches silicon wafer having the structure indicated in FIG. 12 formed on its surface is transferred from an adjacent transfer
10 chamber (not shown in the figure) via the gate valve 16. The left figure in FIG. 12 indicates a cross section 121 before etching. On the silicon wafer 129, the gate oxide film 128 of 4 nm thick is formed, whereon p-type polycrystalline Si film 126 of 100 nm
15 thick and n-type polycrystalline Si film 127 of 100 nm thick are formed in a mixed manner, and further WN film 125 of 10 nm thick and W film 124 of 100 nm thick are formed thereon. On the W film, an oxide film 123 of 100 nm thick, which has been manufactured for
20 patterning with width of 140 nm as an etching mask, is formed. A mixed gas consisting of CF_4 gas 45 ml/min, HBr gas 15 ml/min, O_2 gas 25 ml/min, and N_2 gas 8 ml/min is introduced into the plasma treating chamber 35 through the gas inlet formed on the dielectric 13,
25 and pressure of the gas is maintained at 0.5 Pa. Gas plasma is generated by applying electromagnetic waves of 450 MHz, 600 W, and the W film and the WN film are

etched by applying bias of 400 KHz, 60 W to the process platform 5. The distance (gap) from the wafer 6 placed on the process platform 5 to the dielectric 13, which corresponds to the wafer facing plane, is set as 70 mm.

5 The coil current is adjusted to make the magnetic field intensity 160 Gauss at a position far from the wafer 6 by 60 mm on the wafer, and to make the magnetic field gradient 15 Gauss/cm at the same positions (ECR height). The magnetic field intensity of 160 gauss is

10 a magnetic field intensity to satisfy the ECR condition, and a ratio of magnetic field gradient/magnetic field intensity is 0.09 Gauss/cm. Under the above condition, the thickness of the ECR region corresponding to the high electronic temperature

15 region is approximately 15 mm, and the electronic temperature is approximately 8 eV. The electronic temperature in the region other than the ECR region, which corresponds to the low electronic temperature region, is approximately 2 eV. After etching the W

20 film and the WN film, Cl_2 gas 20 ml/min, HBr gas 80 ml/min, O_2 gas 4 ml/min are introduced into the plasma treating chamber 35, and plasma is generated by applying the electromagnetic waves of 450 MHz, to the atmospheric antenna 34 by 500 W. The ion current

25 density injected into the wafer 6 is approximately 1.5 mA/cm². The power of the high frequency bias applied to the wafer 6 is set at 40 W to perform etching of the

p-type and n-type polycrystalline Si. When the etching is proceeded to the gate oxide film 128, the flow of the Cl gas is stopped, the introducing flow of HBr gas is changed to 70 ml/min, the introducing flow of O₂ gas is changed to 6 ml/min, and the gas pressure is changed to 0.4 Pa.

Because the dissociation of Cl₂ requires an energy of approximately 2.5 eV, the dissociation of Cl₂ is not proceeded in the low electronic temperature region, and the injection amount of Cl radicals are decreased. Therefore, side etching at the side plane of the n-type polycrystalline Si is suppressed significantly, and the n-type polycrystalline Si can be manufactured perpendicularly approximately as same as the p-type polycrystalline Si (the right figure 122 in FIG. 12 indicates the shape after etching). The etching in a depth direction is proceeded by dissociation-adsorption of Cl₂ and ion injection. Therefore, even if the number of the Cl radicals are decreased, the etching velocity is not changed as approximately 200 nm/min. Under the condition that the magnetic field gradient is 0.5 Gauss (the ratio of magnetic field gradient/magnetic field intensity becomes 0.003 Gauss/cm), the high electronic temperature region is extended, and the dissociation of Cl₂ is enhanced. Accordingly, the injection amount of Cl radicals to side plane of the groove is increased, and side etching is readily

generated on the n-type polycrystalline Si. If the flow of O₂ gas is increased to 8 ml/min in order to decrease the side etching, a strong protective film is formed on the side plane of the p-type polycrystalline Si, fattening of the shape (tapered shape) is generated, and obtaining the same perpendicular shape as the n-type polycrystalline Si becomes difficult.

Even if the gas pressure is increased from 0.4 Pa to 0.8 Pa, the perpendicular shape can be obtained. However, if the gas pressure is increased equal to or higher than 1.2 Pa, the fattening is generated in manufactured shape in the isolated pattern. If the gas pressure is decreased to 0.15 Pa, almost similar shape as the etched shape at 0.4 Pa can be obtained. However, if the gas pressure is decreased further lower than 0.1 Pa, the electronic temperature in the low electronic temperature region is elevated, and dissociation of Cl₂ is enhanced. Therefore, decreasing the difference in manufactured shapes of the p-type and the n-type becomes difficult.

After etching the polycrystalline Si, the gas pressure is increased to 0.8 Pa, in order to prevent generation of etching residue, and the polycrystalline Si is treated with HBr gas 90 ml/min, and O₂ gas 7 ml/min for 15 seconds.

As explained above, even in the manufacturing the gate electrode, side etching can be suppressed by

controlling the two electronic temperature regions, and almost similar manufactured shapes can be obtained with both p-type and n-type polycrystalline Si.

Even in the case of manufacturing metallic circuit
5 including Cl_2 gas and BCl_3 gas, the amount of Cl radicals is decreased and perpendicularly manufacturing becomes easy by similarly broadening the low electronic temperature region.

In the case of etching an effective insulating
10 film with N_2 gas and H_2 gas, the etching can be proceeded so as to flatten the bottom plane of the holes or grooves by controlling the two electronic temperature regions so as to make the electronic temperature on the wafer low, because dissociation of
15 reaction products are suppressed and unnecessary accumulation can be avoided. The same result can be obtained with NH_3 gas.

Next, another embodiment using the apparatus indicated in FIG. 1 is explained.

20 Eight inches silicon wafer is transferred into the apparatus as the member to be treated. On the silicon wafer, a gate electrode is formed, whereon a silicon nitride film is formed, whereon an oxide film of 0.7 μm thick is formed, and a resist mask reprinted with a
25 mask pattern is formed thereon. Holes having 250 nm in diameter are formed on the resist mask. Practically, the structure is similar with the cross sectional shape

88 before etching in FIG. 8, and the distance from the upper portion of the oxide film to closest silicon nitride film is approximately $0.4 \mu\text{m}$.

A mixed gas consisting of Ar 400 ml/min, C_4F_8 , and
5 O_2 is introduced into the plasma treating chamber 35 of the apparatus through the gas inlet 24, and the gas pressure is maintained at 2 Pa. Gas plasma is generated with high frequency waves of 450 MHz, 1.3 kW, and etching the oxide film is performed by applying the
10 high frequency bias of 400 KHz, 1000W, to the process platform 5. To the antenna 23, the bias of 400 W is applied from another high frequency power source 20 of 85 KHz. The process platform 5 is set at a position separated from the antenna 23 by 80 mm. The coil
15 current is adjusted to make the magnetic field intensity 160 Gauss at a position far from the wafer 6 by 50 mm on the central portion of the wafer, to make the magnetic field gradient 15 Gauss/cm at the same positions, and to make the magnetic field intensity 160
20 Gauss at a position above the peripheral portion of the wafer by 60 mm. Under the above condition, the thickness of the ECR region corresponding to the high electronic temperature region 101 is approximately 35 mm, and the electronic temperature is approximately 8
25 eV. The electronic temperature in the region other than the ECR region corresponding to the low electronic temperature region 102 is approximately 2 eV. The ion

current density is approximately 5 mA/cm^2 . Under the above condition, the etching treatment is performed using C_4F_8 gas flow in the range from 4 ml/min to 40 ml/min. The flow rate of O_2 was adjusted so that the
5 $\text{O}_2/\text{C}_4\text{F}_8$ ratio becomes 0.5. The etching velocity of the oxide film is increased with increasing the flow rate of C_4F_8 gas.

The injection ratio of $\text{CF}_2/(\text{F} + \text{O})$ and the injection ratio of CF_2/ions onto the wafer depend on
10 the C_4F_8 gas flow rate as indicated by the curve 131 and 132 in FIG. 13, respectively. Here, because O radical etches the silicon nitride film, injection of O is taken into consideration. It is revealed that if the C_4F_8 gas flow rate is small, the silicon nitride
15 film is not protected by CF_2 , and if the C_4F_8 gas flow rate is increased, the silicon nitride film is etched by F and O. The dependency of selection ratio of shoulder portion of the silicon nitride film on the C_4F_8 gas flow rate is indicated by the curve 141 in
20 FIG. 14.

The selection ratio of shoulder portion of the silicon nitride film is decreased by ion spattering at low C_4F_8 gas flow rate, and by etching with F and O at high C_4F_8 gas flow rate. Under the above condition,
25 the optimum high C_4F_8 gas flow rate is in the range approximately from 2 % to 5 %. Under the same condition, if kind of the gas is changed to C_6F_8 , the

C_6F_8 gas flow rate in the range from 1% to 3 % becomes optimum. In FIG. 14, the curve 141 corresponds to the injection ratio of $CF_2/(F + O)$, and the curve 142 corresponds to the injection ratio of $CF_2/ions$. As indicated by the curve 142, the perpendicularity (taper angle) of the manufactured shape is determined by the injection ratio of $CF_2/ions$, and the manufactured shape becomes desirable perpendicular shape at low C_4F_8 gas flow rate.

10 In accordance with the present invention, the generation ratio of CF_2/F can be set or controlled arbitrarily using CF group treating gas. Therefore, oxide film etching, which does not depend significantly on gas pressure and gas flow rate, having a high
15 selection ratio to resist and nitride film becomes possible. By utilizing the present invention, contact holes having a high aspect ratio, and an oxide film having a high selection ratio to resist and silicon nitride film can be manufactured. Because the above
20 etching can be performed under a low gas pressure condition in the range from 1 Pa to 4 Pa, a perpendicularly manufactured shape can be obtained with contact holes having a high aspect ratio.